

# Radiation Damage of Standard and Oxygenated Silicon Diodes by 16 and 27 MeV Protons

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## Abstract

The effects of irradiation by 16 MeV and 27 MeV protons on standard and oxygenated silicon diodes, processed by different technologies, have been investigated. The acceptor creation rate  $\beta$ , after type inversion can be lower for standard diodes than for state of the art oxygenated devices, suggesting that the role of oxygen is more complex than expected and must be folded with the technology of the fabrication process. In addition we show the inaccuracy of the  $\beta$  normalization by the non-ionizing energy loss (NIEL) factor not only for oxygenated diodes but also for standard non-oxygenated devices.

## I. INTRODUCTION

It is well known that under irradiation the presence in silicon of high oxygen concentrations up to  $[O] \approx 2 \cdot 10^{17} \text{ O/cm}^3$  does not affect the volumetric leakage current increase rate  $\alpha$ , which depends on energy and type of radiation, in agreement with the NIEL scaling model [1-6]. On one hand, the acceptor creation rate ( $\beta$ ) after neutron irradiation is not significantly affected by the oxygen concentration [1-4]; on the other hand,  $\beta$  and consequently the depletion voltage ( $V_{\text{dep}}$ ) is dramatically reduced, and by the same amount, in oxygenated diodes irradiated by 24 GeV protons and 192 MeV pions [2-5] whereas this effect is smaller for 27 MeV protons [7]. Oxygen-based models have been proposed to explain the capability of oxygen to suppress the formation of  $V_2O$  centers considered to be responsible for changes in  $V_{\text{dep}}$  after irradiation [8].

The  $\beta$  behavior under charged hadron irradiation shows that the non-ionizing energy loss (NIEL) factors are not sufficient to normalize the acceptor creation rate for oxygenated devices [3,4]. Moreover our group has recently reported that  $\beta$  cannot be scaled by NIEL factors even for standard silicon devices after low energy proton irradiation [9]. In addition, other studies summarized in [10] have shown that  $\beta$  values for standard silicon diodes fabricated with different process can vary significantly, thus confirming the limits of the NIEL hypothesis, whereas oxygenated diodes are less sensitive to the fabrication process and their  $\beta$ s are systematically lower than those of the standard diodes.

In this work we report further on the evidence of the role of processing for what concerns the acceptor creation rate for standard and oxygenated diodes, showing that lower  $\beta$  values can be found for standard devices than for state of the art

oxygenated diodes. In the light of this evidence, oxygen-based models appear to be too restrictive without taking into account other impurities and/or processing step effects, which affect the radiation induced acceptor creation rate.

## II. DEVICES, EXPERIMENTAL CONDITIONS AND ELECTRICAL MEASUREMENTS

The devices tested are state of the art silicon diodes fabricated by ITE [11] and ST Microelectronics [12]. The bulk of all the diodes was initially n-type with resistivity of 1.3–3 k $\Omega$ ·cm. The active area is surrounded by a  $n^+$  guard-ring. The ITE devices were provided to us by the ROSE collaboration [13]. They were processed in both standard ( $[O]_{\text{standard}} < 4 \cdot 10^{16} \text{ cm}^{-3}$ ) and oxygenated ( $[O]_{\text{oxygenated}} > 10^{17} \text{ cm}^{-3}$ ) Si substrates. The standard diodes were obtained from wafers produced by Polovodice (PV) [14]. The oxygenated devices (JO) were processed on wafers by ITME [15]: oxygen was introduced by a jet of gas during the refining process. The ST Microelectronics diodes (ST) were processed on wafers with standard oxygen concentrations from Waker [16].

The geometrical dimensions and the oxygen and carbon concentrations of the PV and JO diodes, measured by SIMS at EVANS [17], are summarized in Table 1 along with data provided to us by ST. A new SIMS analysis of the carbon and oxygen content of the ST diodes is underway.

Table 1  
Typical diode characteristics.

	PL	JO	ST
Area (cm <sup>2</sup> )	0.25	0.25	0.25
Thickness ( $\mu\text{m}$ )	285	307	305
[O] (cm <sup>3</sup> )	$< 4 \cdot 10^{16}$	$2.1\text{-}2.3 \cdot 10^{17}$	$< 4 \cdot 10^{16}$
[C] (cm <sup>3</sup> )	$9 \cdot 10^{15}$	$1 \cdot 10^{16}$	$\leq 9 \cdot 10^{15}$

Irradiations were performed in two periods at the SIRAD irradiation facility of the Tandem accelerator at the INFN Laboratori Nazionali di Legnaro (Padova, Italy) [18]. In the first (second) period the standard PV and the oxygenated JO diodes (the standard PV and ST devices) were irradiated; i.e. the PV diodes were considered as reference devices.

During each period all the diodes were simultaneously irradiated without bias in cumulative steps at room temperature. At least two diodes of the same type were irradiated in the same experimental conditions: a proton (p) beam of 27 MeV was rastered with a uniformity of a few percent across the sample holder where the diodes were

arranged in two rows. The diodes of one row received directly the 27 MeV protons; the other diodes were placed immediately behind a 2.45 mm thick silica strip that degrades the proton energy down to 15.7 MeV (FWHM $\approx$ 0.7 MeV). This energy is still large enough to guarantee a uniform energy loss along the proton path in a  $\approx$ 300  $\mu$ m thick silicon diode. The fraction of protons scattered by the silica strip away from the diodes in the low energy row is calculated to be negligible. The energy degradation and the scattering estimate due to the silica strip were evaluated with SRIM [19].

The proton flux was measured on-line by a square 3-by-3 battery of independent small Faraday cups positioned 10 cm behind the target plane. A fluence of  $10^{13}$  p/cm $^2$  is typically accumulated in 15 minutes; the initial fluence ( $\Phi > 3 \cdot 10^{13}$  p/cm $^2$ ) was chosen so that the diodes were type inverted.

After each irradiation step the devices were thermally annealed at 80°C for 4 minutes in order to complete the beneficial annealing for the depletion voltage  $V_{dep}$  [1-5]. After annealing the devices were characterized by current-voltage (I-V) and 1 kHz, 10 kHz and 100 kHz capacitance-voltage (C-V) measurements by a HP4142 B modular DC source monitor and a HP4284A LCR meter, respectively. During the electrical characterization the reverse bias voltage ( $V_{bias}$ ) was applied to the backside contact, while the n $^+$  guard-ring was grounded.

### III. EXPERIMENTAL RESULTS: PV AND JO DIODES

The depletion voltage used in reporting the following results is defined as the intersection point of the two different slopes on a log-log scale of the 10 kHz C-V curve, as shown in Figure 1 for a standard PV diode after receiving 27 MeV protons for a cumulative delivered fluence of  $9 \cdot 10^{13}$  p/cm $^2$ . The C-V curves of the oxygenated JO devices show the same shape of the PV diodes.

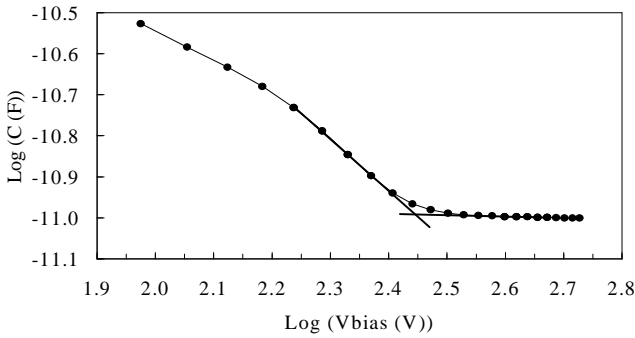


Figure 1. C-V measurement at 10 kHz for a PV diode after the cumulative delivered 27 MeV proton fluence of  $9 \cdot 10^{13}$  p/cm $^2$ .

The effective doping concentration  $N_{eff}$  has been calculated by:

$$N_{eff} = \frac{2\epsilon}{qW^2} V_{dep} \quad (1)$$

where  $W$  is the thickness of the diode,  $\epsilon$  is the absolute Si dielectric constant and  $q$  is the electron charge.

The  $N_{eff}$  data versus the cumulative delivered fluence  $\Phi$  for PV and JO diodes, irradiated by 16 MeV and 27 MeV protons, are shown in Figure 2. As expected,  $N_{eff}$  increases linearly by increasing  $\Phi$ , being the diode substrate type inverted just before the first irradiation step. The acceptor creation rate  $\beta$ , that is the slope of the  $N_{eff}(\Phi)$  curve after substrate inversion, is lower for oxygenated diodes at both proton energies. Moreover  $\beta$  depends on the proton energy in a sizeable way and is lower for 16 MeV protons, whereas the NIEL is expected to increase by decreasing the proton energy [20].

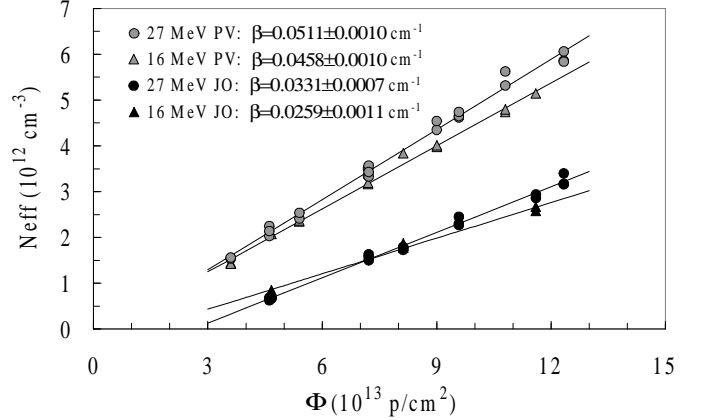


Figure 2.  $N_{eff}$  for PV (dashed symbols) and JO (close symbols) diodes as a function of the cumulative delivered fluence for 27 MeV (circles) and 16 MeV (triangles) protons. The solid lines are linear fits of the experimental data; the  $\beta$  parameters are also reported.

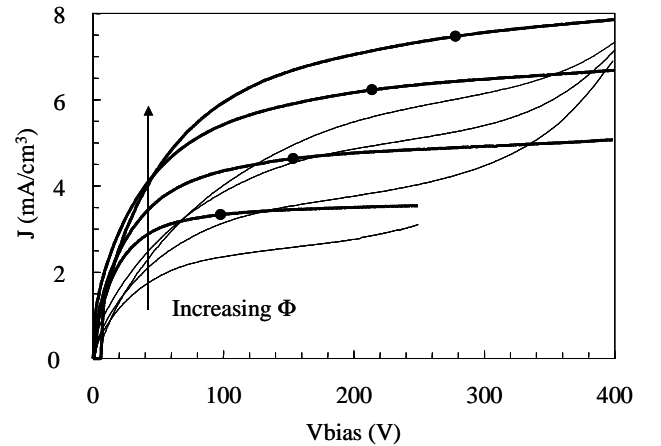


Figure 3. Diode (solid thick line) and guard-ring (solid thin line) current densities normalized to 20°C for PV devices irradiated by 27 MeV protons at  $\Phi_1 = 3.6 \cdot 10^{13}$  p/cm $^2$ ,  $\Phi_2 = 5.4 \cdot 10^{13}$  p/cm $^2$ ,  $\Phi_3 = 7.2 \cdot 10^{13}$  p/cm $^2$  and  $\Phi_4 = 9 \cdot 10^{13}$  p/cm $^2$ . The circles on the four diode curves mark the diode current density at full depletion.

The current densities  $J=I/Vol$ , where  $I$  and  $Vol$  are the currents and the volume of the diode, respectively, have been normalized to 20°C by considering the temperature dependence [21]  $J(T)=AT^2 \cdot \exp(-E/2k_B T)$ , where  $A$  is a constant,  $T$  is the absolute temperature,  $k_B$  is the Boltzmann constant and  $E=1.24$  eV.

The diode ( $J_D$ ) and guard-ring ( $J_{GR}$ ) current densities normalized to 20°C are shown in Figure 3 for a PV diode as a function of  $V_{bias}$ , at each cumulative delivered fluence after

27 MeV proton irradiation. As expected,  $J_D$  monotonically increases by increasing  $V_{bias}$ ,  $V_{dep}$  is within the low slope region of the J-V curve and  $J_{GR}$  is lower than  $J_D$  even beyond full depletion. Similar results were obtained for the JO diodes.

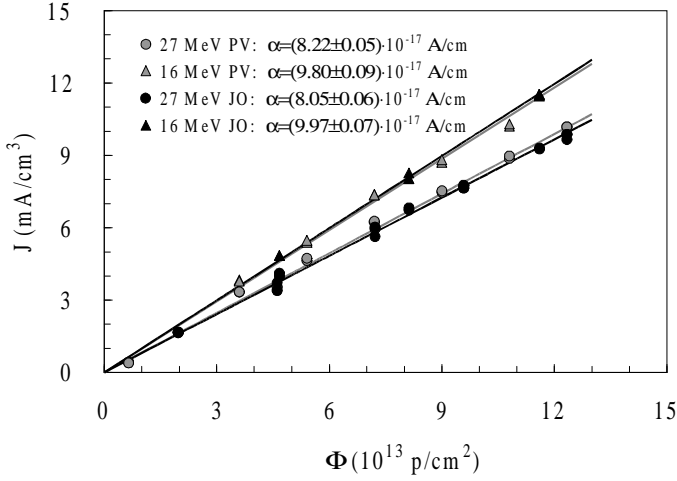


Figure 4.  $J_D$  normalized to 20°C at full depletion for PV (dashed symbols) and JO (close symbols) diodes as a function of the 27 MeV (circles) and 16 MeV (triangles) cumulative delivered proton fluence. The solid lines are linear fits of the experimental data; the  $\alpha$  parameters are also reported.

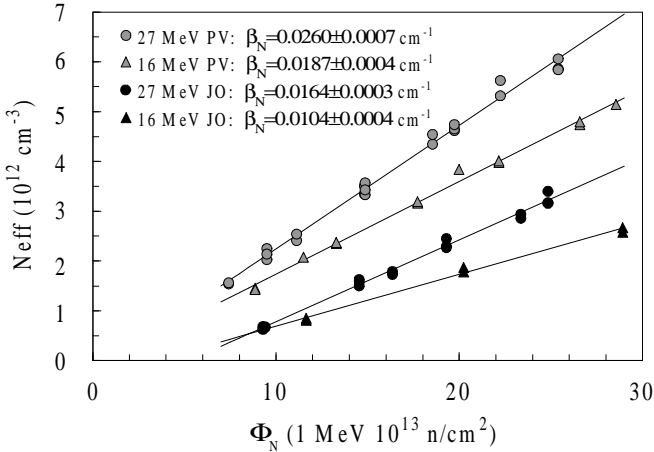


Figure 5.  $N_{eff}$  as a function of 1 MeV neutron equivalent fluence for PV (dashed symbols) and JO (close symbols) diodes irradiated by 27 MeV (circles) and 16 MeV (triangles) protons. The solid lines are linear fits of the experimental data; the  $\beta_N$  parameters are also reported.

The  $J_D$  data measured at  $V_{dep}$  and normalized to 20°C as a function of  $\Phi$  are shown in Figure 4 for PV and JO diodes. As expected,  $J_D$  is proportional to the cumulative delivered fluence; i.e.  $J_D = \alpha\Phi$ . The volumetric leakage current increase rate  $\alpha = \alpha(X, E_x)$  depends on the radiation type  $X$  and on its energy  $E_x$  but it does not depend on the device oxygen concentration. The  $\alpha$  parameter is higher for 16 MeV protons in agreement with the NIEL scaling hypothesis:

$$\alpha(X, E_x) / \alpha(Y, E_y) = k(X, E_x) / k(Y, E_y) \quad (2)$$

where  $k$  is the hardness factor [21] of radiation  $X$  at energy  $E_x$ . By using the experimentally determined values of  $\alpha$  at a

standard temperature of 20°C, shown in Figure 4, the 27 MeV and 16 MeV cumulative delivered proton fluences have been normalized to the 1 MeV neutron equivalent fluence ( $\Phi_N$ ) by:

$$\Phi_N = \Phi \frac{\alpha(\text{proton}; E)}{\alpha(\text{neutron}; 1 \text{ MeV})} \quad (3)$$

where  $\alpha(\text{neutron}, 1 \text{ MeV}) = 4 \cdot 10^{-17} \text{ A/cm}$  [6].

After normalization, the  $N_{eff}$  data for 16 MeV and 27 MeV protons, as a function of  $\Phi_N$  (see Figure 5), do not overlap for both standard and oxygenated diodes, confirming that the  $\beta$  parameter does not scale by the NIEL factor not only for oxygenated but also for standard devices, at least for low energy protons. The slope of the  $N_{eff}(\Phi_N)$  line, that is the  $\beta_N$  parameter, is smaller for the JO diodes, and for a fixed device type it is lower for devices irradiated by 16 MeV protons. This suggests that there is a similar energy dependence for a given oxygen concentration. In particular the energy dependence of  $\beta_N$  for PV diodes indicates that the suppression of acceptor creation occurs at low proton energy even with very small oxygen concentrations.

#### IV. EXPERIMENTAL RESULTS: ST DIODES

The ST diodes show a somewhat peculiar behaviour. At high cumulative delivered fluences ( $> 6 \cdot 10^{13} \text{ p/cm}^2$ ) the C-V curves at the standard 10 kHz frequency used to determine  $V_{dep}$  present an anomalous peak structure completely absent in the standard PV and JO diodes (see Figure 6). The structure grows with fluence and is more pronounced for C-V measurements at 1 kHz, while it is practically absent at 100 kHz. This structure may introduce a systematic error in the  $V_{dep}$  determination at the highest fluences, which nevertheless is expected to be small in our analysis because the linear fit of the C-V curve in the low slope region is well outside of the peak region, as shown in Figure 6.

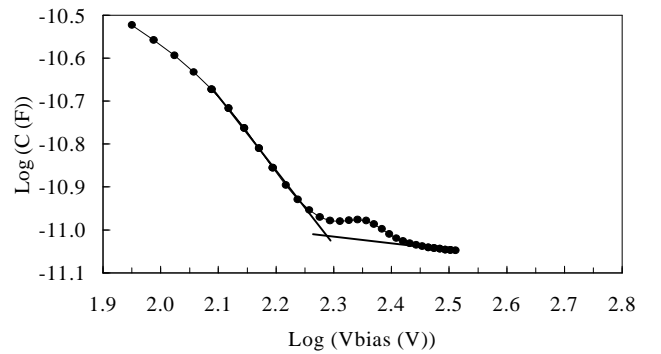


Figure 6: C-V measurement at 10 kHz for a ST diode after the cumulative delivered 27 MeV proton fluence of  $9 \cdot 10^{13} \text{ p/cm}^2$ .

The  $N_{eff}(\Phi)$  curves determined by the C-V measurements for the ST diodes are shown in Figure 7: the  $\beta$  parameter is lower for devices irradiated by 16 MeV protons, as already observed with the PV and JO diodes. The standard ST  $N_{eff}(\Phi)$  curves are surprisingly close to the data shown in Figure 2 for the oxygenated JO devices. Even though the two ST diodes irradiated by 27 MeV protons show a small data

dispersion,  $\beta$  is lower for standard ST diode than for state of the art oxygenated devices. This suggests that other impurities and/or effects in processing steps affect the radiation hardening of the final device in order to obtain low  $\beta$  values.

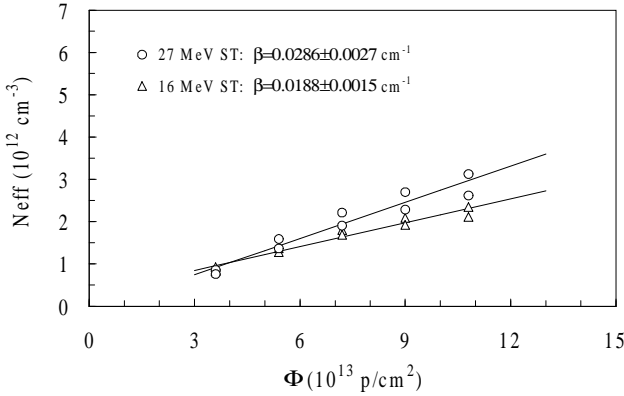


Figure 7:  $N_{eff}$  for ST diodes as a function of the cumulative delivered fluence for 27 MeV (circles) and 16 MeV (triangles) protons. The solid lines are linear fits of the experimental data; the  $\beta$  parameters are also reported.

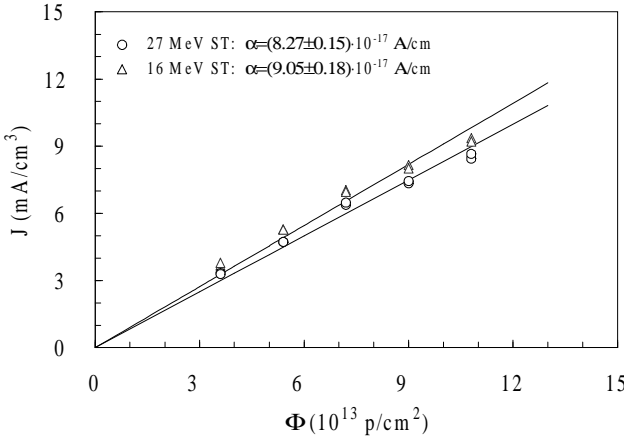


Figure 8:  $J_d$  normalized to 20°C at full depletion for ST diodes as a function of the 27 MeV (circles) and 16 MeV (triangles) cumulative delivered proton fluence. The solid lines are linear fits of the experimental data; the  $\alpha$  parameters are also reported.

The correlation  $J_d$  at  $V_{dep}$  of the ST diodes as a function of  $\Phi$ , shown in Figure 8, is not as good as that obtained for PV and JO diodes (see Figure 4): the experimental data seem to deviate from linearity at the highest fluences. In addition the ST  $\alpha$  values disagree somewhat with the PV and JO data, even if the ST  $\alpha$  is again higher for the 16 MeV proton irradiated diodes, as in Figure 4. The peculiarities of the ST  $\alpha$  values are due to the anomalous behavior of the diode and guard-ring currents (see Figure 9), which affects the  $J_d$  measurement at  $V_{dep}$ , especially for high fluences. We recall that  $J_{GR}$  is lower than  $J_d$  in PV and JO diodes up to  $V_{bias}$  values significantly higher than  $V_{dep}$ , and  $J_d$  monotonically increases by increasing  $V_{bias}$  (see Figure 4). On the contrary, the ST  $J_{GR}$  (Figure 9) starts to increase quickly at values of  $V_{bias}$  the nearer to  $V_{dep}$  the higher the received fluence, reaching 50 mA/cm<sup>2</sup> at 400 V. Correspondingly the diode current density  $J_d$  decreases. These anomalous behaviors indicate that our measurements do not well estimate  $J_d$  at  $V_{dep}$  by an amount which increases with the fluence. Using the face values of

$V_{dep}$  obtained with the standard procedures used for the PV and JO diodes, we obtain the results plotted in Figure 8.

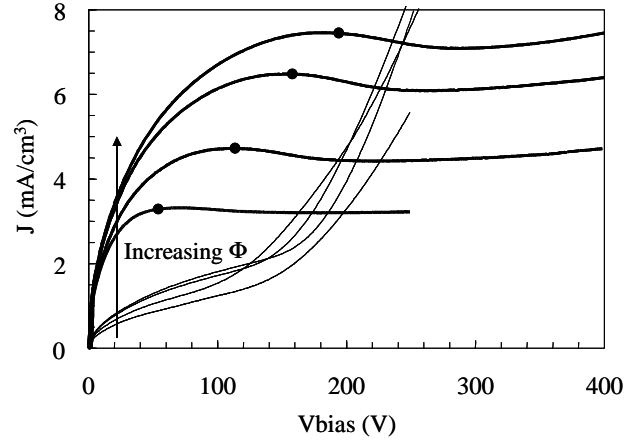


Figure 9: Diode (solid thick line) and guard-ring (solid thin line) current densities normalized to 20°C for ST devices irradiated by 27 MeV protons at  $\Phi_1=3.6 \cdot 10^{13}$  p/cm<sup>2</sup>,  $\Phi_2=5.4 \cdot 10^{13}$  p/cm<sup>2</sup>,  $\Phi_3=7.2 \cdot 10^{13}$  p/cm<sup>2</sup> and  $\Phi_4=9 \cdot 10^{13}$  p/cm<sup>2</sup>. The solid circles on the four diode curves mark the diode current density at full depletion.

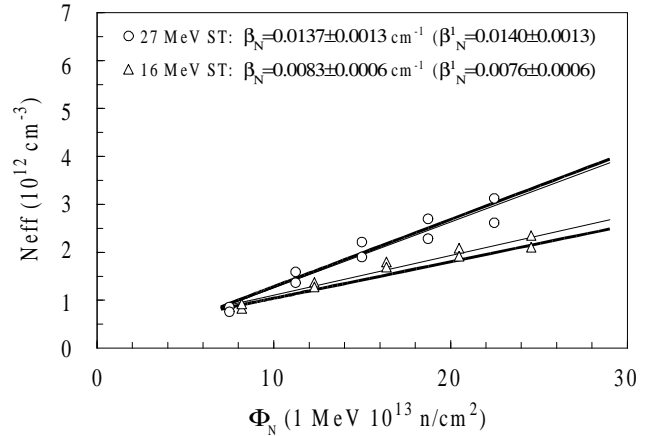


Figure 10:  $N_{eff}$  for ST diodes as a function of the 1 MeV neutron equivalent fluence. Devices were irradiated by 27 MeV (circles) and 16 MeV (triangles) protons. The thin solid lines are linear fits of the experimental data; the  $\beta_N$  parameters are also reported. The thick solid lines are linear fits, whose  $\beta_N^1$  parameters are also reported, obtained by normalizing the 27 MeV (16 MeV) proton fluence to 1 MeV neutron by considering the average value of all the 27 MeV (16 MeV) PV and JO  $\alpha$  values.

The values of  $\beta_N$  obtained for the ST diodes by considering the  $\alpha$  values of Figure 6 for normalization of the proton fluence to the 1 MeV neutron equivalent value are shown in Figure 10. In the same figure we also report the fits which are obtained if the proton fluence normalization is performed by considering the average  $\alpha$  value of the PV and JO diodes irradiated by protons with the corresponding energy. The slopes  $\beta_N^1$  of these fits are compatible with the above  $\beta_N$  within the fitting parameter error. In spite of the reported difficulties in determining  $V_{dep}$  and  $J_d$  at full depletion, the data of the ST diodes present qualitatively the same energy dependence of  $\beta_N$  shown for the standard PV and oxygenated JO diodes. However standard ST diodes have values of  $\beta_N$  that are

significantly small, even smaller than those of the oxygenated JO devices.

## V. CONCLUSIONS

We have shown that, in silicon diodes irradiated by 27 MeV and 16 MeV protons, the acceptor creation rate  $\beta$ , after type inversion, is sensitive to the energy of the impinging particles also for standard (non-oxygenated) material. This effect is amplified when the delivered fluences are normalized to the 1 MeV neutron equivalent values in disagreement with the currently accepted NIEL hypothesis. The  $\beta$  parameter decreases in a significant way when the proton energy is lowered by 27 MeV to 16 MeV. It is worth noting that on the contrary the leakage current damage constant  $\alpha$  is independent of the oxygen content and increases by lowering the proton energy, in good quantitative agreement with NIEL expectations.

When processed the same way, oxygenated diodes show a lower acceptor creation rate than the standard ones, the effect being lower of a factor 2-3 at these proton energies than for 24 GeV protons.

However standard diodes fabricated from silicon wafers of similar characteristics (in particular resistivity) with a different process show an acceptor creation rate which can be lower than that of highly oxygenated diodes.

A further comparison of the behavior of standard and oxygenated ST diodes is underway. The data of the ST diodes presented here indicate, at least qualitatively, that the role of oxygen in affecting the acceptor creation rate is not yet completely understood. High oxygen concentrations play an important role in improving the hardening of the starting material, but the effects of other impurities and/or processing steps can be quite important in changing the acceptor creation rate  $\beta$  and in assessing the radiation hardness of silicon detector. Therefore these effects must be systematically investigated in order to understand the behavior of the low  $\beta$  standard silicon devices.

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